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NASA CR

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GENERAL ELECTRIC

HOUSTON, TEXAS

TECHNICAL INFORMATION RELEASE

TIR 741-MED-4011

FROM D. J. Grounds		TO J. A. Rummel, Ph.D./DB6	
DATE 7/17/74	WORK ORDER REF: DM-110T	WORK STATEMENT PARA: NAS9-12932	REFERENCE:

SUBJECT

Transient Thermoregulatory Model with Graphics Output

(NASA-CR-160217) TRANSIENT THERMOREGULATORY  
MODEL WITH GRAPHICS OUTPUT (General Electric  
Co.) 25 p HC A02/MF A01 CSCI 06P

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G3/52 22235

This report is a user's guide for the transient version of the thermoregulatory model of Stolwijk. The model is designed to simulate the transient response of the human thermoregulatory system to thermal inputs. The model consists of 41 compartments over which the terms of the heat balance are computed. The control mechanisms which are identified are sweating, shivering, vasoconstriction and vasodilation.



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Attachment

/db

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## PROGRAM DESCRIPTION

### A. IDENTIFICATION

Program Name - Thermoregulatory Model of Stolwijk (Transient Version)  
Bioengineer Contact - D. J. Grounds  
Programmer - V. J. Marks  
Date of Issue - June 30, 1974

### B. GENERAL DESCRIPTION

This user's guide and program description updates and replaces TIR 741-MED-3011. The model is designed to simulate the transient response of the human thermoregulatory system to thermal inputs. The model consists of 41 compartments over which the terms of the heat balance are computed. The control mechanisms which are identified are sweating, shivering, vasoconstriction and vasodilation.

### C. USAGE AND RESTRICTIONS

Machine and Compiler Required - Univac 1110 TSS and FORTRAN V  
Peripheral Equipment Required - Time Sharing Terminal  
- Tektronix 4010 Graphics Terminal

### D. PARTICULAR DESCRIPTION

A detailed description of the basic model is given in references 1-5. The current modifications include an improved shivering mechanism and the introduction of a graphics output option.

The shivering mechanism which appeared in earlier versions was described by the following equation.

$$QSHIV = CCHIL * COLD(1) + SCHIL * COLDS + PCHIL * COLD(1) * COLDS.$$

But, since  $CCHIL = 0.0$  and  $SCHIL = 0.0$ , the expanded equation becomes

$$QSHIV = 12.22 (T_{core\ set} - T_{core}) \text{ head} * (\sum K(1) * (T_{set}(1) - T(1)))$$

where I equals all skin compartments and  $K(1)$ 's are constants based on the weighted mass of each skin compartment. This equation was based on the widely accepted data of Benzinger and Kitzinger(6). However, the data are presented with average skin temperature as an independent

variable. This does not allow verification of the model equation because of the introduction of set point temperatures for each skin compartment. The improved modeling of this mechanism is complicated by several factors. First, although the role of hypothalamic temperature signal and skin temperature signal has each been established as necessary for shivering, the functional relationship for the combined effect of skin receptor signal with hypothalamic signal is unknown for conditions other than uniform skin temperature. Further, the heat that is generated by chemical reactions as a response to cold, chemical thermogenesis is initiated by the same control signals and is therefore extremely difficult to separate from shivering thermogenesis. Shivering can also be initiated through the higher centers as a general sympathetic response. Also, there is considerable variation in the shivering responses between male and female subjects. These factors have contributed to the lack of an accepted control system model of the shivering mechanism.

In order to make the best use of available data without making assumptions which seriously limit the accuracy of the model, the approach chosen was to derive an empirical relationship from the experimental data. This approach was also taken by Riggs (7), but acceptable correspondence to the data could not be obtained using his equations. Although this approach seems to fulfill the requirements of the model, it should be reviewed whenever a more complete understanding of the mechanisms of this process is gained.

By using a combination of linear and parabolic regression schemes based on least squares criterion, a set of equations was found to approximate the curves of reference 6, page 649. These equations are:

$$XTC = TC - (.1 ((37.0 - TC) 1.7)^2) / 10 \quad (1)$$

$$RM = 22221. - 614.2 (XTC) + TS (-1933.2 + 53.66 (XTC)) + TS^2 (46.45 - 1.289 (XTC)) \quad (2)$$

$$QSHIV = RMS - QBASAL \geq 0.0 \quad (3)$$

where

QSHIV = Rate of heat produced by shivering BTU/HR

QBASAL = Basal Metabolic Rate BTU/HR

RM = Metabolic Rate CAL/SEC

RMX = Metabolic Rate BTU/HR

TC = Intercranial Temp. °C

TS = Average Skin Temp. °C

The fitted curves are shown in Figure 1 with corresponding experimental data.

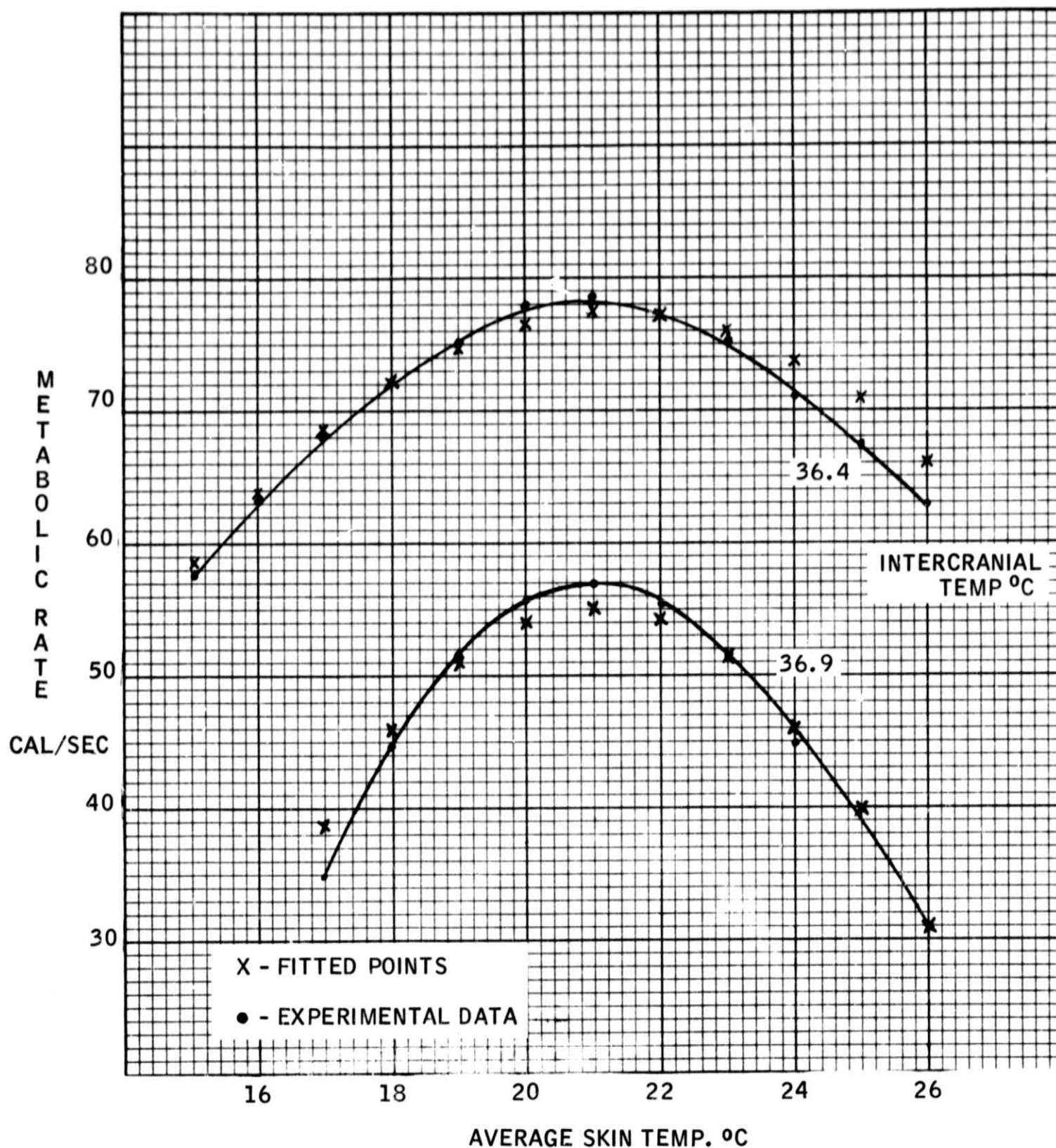


Fig. 1 COMPARISON OF EXPERIMENTAL DATA TO FITTED DATA

## E. DESCRIPTION OF INPUT

The user must specify if the graphics output capability is required. If graphics is required, then a list of variables to plot is solicited. Upon completion of the list a name list input is requested. This request is answered as shown in the example of Appendix 2 by supplying the following values:

Col. 2

RM	Total Metabolic Rate	BTU/HR
QBS	Basal Metabolic Rate	BTU/HR
VEFF	Efficiency of useful work	%
AC	Surface Area for Convection	FT <sup>2</sup>
AR	Surface Area for Radiation	FT <sup>2</sup>
TCAB	Temperature of the Cabin	°F
TW	Temperature of the Walls	°F
TDEWC	Dew Point Temp. in Cabin	°F
VCAB	Cabin Free Stream Velocity	FT <sup>3</sup> /SEC
VEFF	Ventilation Efficiency	%
PCAB	Atmospheric Pressure in Cabin	PSIA
G	Gravity Normal to Earth	
CLOV	Clothing Thickness/Conductivity	FT <sup>2</sup> HR °F/BTU
EUG	Emissivity of Undergarment	
CPG	Specific Heat of Gas	BTU/lb °F
DT	Integration Step Size (.05)	MIN
PRINTI	Print Interval	MIN
SETI	Max Time/Run	MIN
MCASES	Number of Imposed Case	

MCASES = 0 Initial Conditions (Not plotted)

MCASES > 0 Imposed Case Using Final Values for Starting Point

To complete the namelist, input a \$ END is entered beginning in column 2.

## F. DESCRIPTION OF OUTPUT

See Appendix for example output. The graphics output option which has been added to the program is demonstrated in the example run shown. It includes some conversational input to specify the variables to plot and their ranges. There are 55 variables which can be used with the graphics option:

1-43		Temperatures of the T Array (See TIR 741-MED-3011)	°F
44	TUGAV	Average Temperature of Undergarment	°F
45	SQUG	Sum of Sensible Heat Transfer Rate	BTU/HR
46	QEVAP	Heat Transfer Rate of Evaporation from Surface	BTU/HR
47	TOTL	Total Latent Heat Transfer Rate	BTU/HR
48	TDEWC	Dew Point Temp. in Cabin	BTU/HR
49	WORK	The Metabolic Work Performed	°F
50	QSHIV	Heat Produced by Shivering	BTU/HR
51	STOR/T	The Rate of Heat Accumulation	BTU/HR

52	QSTOR	Total Heat Accumulated	BTU/HR
53	TCAB	Temperature of the Cabin	BTU
54	VPDEW	Vapor Pressure at Cabin Dew Point	°F
55	U	Useful Work Performed	BTU/HR

G. INTERNAL CHECKS AND EXITS

The model will proceed until a steady-state condition is met (Storat - Oldstor/Storat)  $\leq .01$  or until maximum time is exceeded whenever MCASES = 0. The model is then initialized with the steady-state values and thermal transients are then simulated for MCASES > 0.

H. INDEPENDENT SUBROUTINES

The Independent Subroutines are MANT, SHRT, VPT, CQSH, TCF, GVAR, and the Tektronix Plot Package. The Subroutines are listed in Appendix 1.

I. SYSTEM SUBROUTINES

No special system routines are required.

J. COMPLETION DATE

June 25, 1974

REFERENCES

1. "41-Node Transient Metabolic Man Program", LEC/672-23-030031, Lockheed Electronics Company, Houston Aerospace Systems Division.
2. "Simplification of 1108 Lockheed Version of Stolwijk Model and Incorporation of Improved Convective Heat Transfer Coefficient", TIR 750-MED-2002, General Electric Company, Space Division, Houston Programs and a revision, TIR 741-MED-2004.
3. "Incorporation of Basal Metabolic Rate as an Input Parameter", TIR 750-MED-2003, General Electric Company, Space Division, Houston Programs and a revision, TIR 750-MED-2005.
4. "Incorporation of Clothing Logic Contained in Stolwijk Amoeba Program into Simplified Lockheed Version of Stolwijk Model", TIR 750-MED-2006, General Electric Company, Space Division, Houston Programs.
5. "Steady State Version of Lockheed Program", TIR 741-MED-2011, General Electric Company, Space Division, Houston Programs.
6. Benzinger, T.H. and Kitzinger, C., "The Human Thermostat", Temperature Part 3 - Medicine and Biology, Reinholdt Publishing Corp., New York, 1963.
7. Riggs, D.S., Control Theory and Physiological Feedback Mechanisms Williams and Wilkins Co., Baltimore, Md., 1970, p. 388.



APPENDIX 1  
PROGRAM LISTING

DEFINITION OF BODY SEGMENT TEMPERATURE SUBSCRIPTS			
T(1)	= HEAD CORE	T(2)	= HEAD MUSCLE
T(3)	= HEAD FAT	T(4)	= HEAD SKIN
T(5)	= TRUNK CORE	T(6)	= TRUNK MUSC
T(7)	= TRUNK FAT	T(8)	= TRUNK SKIN
T(9)	= RIGHT ARM CORE	T(10)	= RIGHT ARM MUSCLE
T(11)	= RIGHT ARM FAT	T(12)	= RIGHT ARM SKIN
T(13)	= LEFT ARM CORE	T(14)	= LEFT ARM MUSCLE
T(15)	= LEFT ARM FAT	T(16)	= LEFT ARM SKIN
T(17)	= RIGHT LEG CORE	T(18)	= RIGHT LEG MUSCLE
T(19)	= RIGHT LEG FAT	T(20)	= RIGHT LEG SKIN
T(21)	= LEFT LEG CORE	T(22)	= LEFT LEG MUSCLE
T(23)	= LEFT LEG FAT	T(24)	= LEFT LEG SKIN
T(25)	= RIGHT HAND CORE	T(26)	= RIGHT HAND MUSCLE
T(27)	= RIGHT HAND FAT	T(28)	= RIGHT HAND SKIN
T(29)	= LEFT HAND CORE	T(30)	= LEFT HAND MUSCLE
T(31)	= LEFT HAND FAT	T(32)	= LEFT HAND SKIN
T(33)	= RIGHT FOOT CORE	T(34)	= RIGHT FOOT MUSCLE
T(35)	= RIGHT FOOT FAT	T(36)	= RIGHT FOOT SKIN
T(37)	= LEFT FOOT CORE	T(38)	= LEFT FOOT MUSCLE
T(39)	= LEFT FOOT FAT	T(40)	= LEFT FOOT SKIN
T(41)	= CENTRAL BLOOD	T(42)	= AVERAGE SKIN
T(43)	= AVERAGE MUSCLE		

ORIGINAL PAGE  
OF POOR QUALITY

```

30 FORMAT(/'INPUT DATA USING NAMELIST $INPUT'//)
READ(5,INPUT)
QBASAL=QBS
IF(QBASAL.LT.0.01) QBASAL=293.
IF(QBASAL.GT.RM) QBASAL=RM
WRITE(6,INPUT)
IF(MCASES.EQ.0) WRITE(6,60)
60 FORMAT(1H0,17X,18HINITIAL CONDITIONS//)
IF(MCASES.NE.0) WRITE(6,80)
80 FORMAT(1H0,17X,18HIMPOSED CONDITIONS//)
DTIME=DT/60.
SETX=SETI/60.
IF(NKPLT.EQ.1.AND.MCASES.GT.0) KPLT=1
SETT=SETX
PRINT=PRINTI/60.

```

```

C.....
C
C  INITIALIZATION
C
C.....

```

```

PRNOW=PRINT
IF(MCASES.GT.0) GO TO 140
IF(ICOND.EQ.1.AND.MCASES.EQ.0) WRITE(6,654)
654 FORMAT(' NOT INITIALIZED AT STEADY STATE')

```

```

KPLT=0

```

```

ICOND=0

```

```

KOUNT=0

```

```

QLCG=0.

```

```

SQUG=0.

```

```

QEVAP=0.

```

```

TOTL=0.

```

```

QSHIV=0.

```

```

QSTOR=0.

```

```

STORAT=0.

```

```

DO 100 I=1,43

```

```

100 T(I)=TSET(I)

```

```

TUGAV=T(42)

```

```

DO 120 I=1,10

```

```

J=4*I

```

```

120 TUG(I)=T(J)

```

```

C.....

```

```

140 DO 160 I=1,10

```

```

J=4*I

```

```

ACE(I)=PCA(I)*AC

```

```

ARE(I)=PCA(I)*AR

```

```

160 CONTINUE

```

```

STIME=STIME+TIME

```

```

TIME=0.

```

```

U=UEFF/100.*(RM-QBASAL)

```

```

WORK=RM-QBASAL-U

```

```

VPDEW=VPT(TDEWC)

```

```

CLO=.88*CLOV

```

```

180 CONTINUE

```

```

200 FORMAT(125H1 TIME

```

```

1Q EVAP Q LATENT HEAT

```

```

2 , / 125H MIN

```

```

3BTU/HR BTU/HR STORAGE

```

```

TEMP

```

```

SHIVER

```

```

HEAD

```

```

RATE

```

```

AV TEMP

```

```

TOTL CABIN

```

```

SKIN,

```

```

HEAT TEMP

```

```

TEMP

```

```

DEW

```

```

UNDER=

```

```

POINT

```

```

Q

```

```

SENSIBLE

```

```


```

```


```

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4	/ 125H		CORE	F	GARMENT	BTU/HR
5		RATE	BTU/HR	STORAGE	F	
6	/ 98H		F		F	
7		BTU/HR		BTU/1		

LC=7

C.....

WRITE(6,789)

789 FORMAT(1H,3X,'THINS',11X,'HEADCORE',AVGSKIN,TUGAV,BLOOD,QE

CVAP,INSENS,STORAT,QSHIV,QSTOR,TCAB,TDEWC)

C MAIN LOOP FOR SHIRTSLEEVE CASE

C.....

220 PTIM=TIME\*60.

IF (LC.GT.58) GO TO 180

LC=LC+1

IF (MCASES.EQ.0) GO TO 567

NBUF=NBUF+1

IF (NBUF.GT.181) NBUF=181

XBUF(NBUF)=PTIM

DO 230 I=1,NN

NI1=NI(I)

230 YBUF(NBUF,I)=PLT(NI1)

IF (KPLT.GT.0) CALL PLOTX

IF (KPLT.GT.0) GO TO 260

567 CONTINUE

C WRITE(6,2)TAVG,RMX,TC,QSHIV

2 FORMAT(1H,5X,'SKINT=',F11.5,5X,'MET RATE=',F11.5,

65X,'I-C TEMP=',F11.5,5X,'QSHIV=',F11.5)

C DO887 IL=1,33,8

C887 WRITE(6,888)(QCONV(IL+1,ILL),ILL=1,8)

888 FORMAT(8F9.2)

WRITE(6,240)PTIM,T(1),T(42),TUGAV,T(41),QFVAP,TOTL,STORAT,

6 QSHIV,QSTOR,TCAB,TDEWC

240 FORMAT(F8.1,9X,11F9.2)

260 OLDSTR = STORAT

C-----

C

CALL SHRT

C-----

C

TIME=TIME+DTIME

IF (ABS(STORAT).GT.2.) GO TO 280

IF (ABS((OLDSTR-STORAT)/STORAT).LT..001) GO TO 300

280 IF (TIME.GE.SETT) GO TO 300

IF (MCASES.EQ.0) GO TO 260

IF (PRNOW.GT.TIME) GO TO 260

PRNOW=PRNOW+PRINT

GO TO 220

300 PTIM=TIME\*60.

PRNOW=TIME+DTIME

IF (MCASES.EQ.0) GO TO 568

NBUF=NBUF+1

IF (NBUF.GT.181) NBUF=181

XBUF(NBUF)=PTIM

DO 310 I=1,NN

NI1=NI(I)

310 YBUF(NBUF,I)=PLT(NI1)

IF (KPLT.GT.0) CALL PLOTX

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```

      IF (KPLT.GT.0) GO TO 315
568 CONTINUE
      WRITE (6,240)PTIM,T(1),T(42),TUGAV,T(41),QEVAP,TOTL,STORAT,QSHIV,
      *QSTOR,TCAB,TDEWC
315 KOUNT=KOUNT+1
      IF (ICOND.EQ.1.AND.KOUNT.LE.MCASES) GO TO 380
C     SAVE INITIAL CONDITION RESULTS TO START IMPOSED CONDITION CASES
320 DO 340 I=1,43
      SAVT(I)=T(I)
340 CONTINUE
      DO 360 I=1,10
      SAVTUG(I)=TUG(I)
360 CONTINUE
      XTUGAV=TUGAV
      XSQUG=SQUG
      XQEVAP=QEVAP
      XTOTL=TOTL
      XSTRAT=STORAT
      XQSHIV=QSHIV
      XQSTOR=QSTOR
      ICOND=1
      GO TO 20
C
C     RESTORE INITIAL CONDITION RESULTS FOR NEXT CASE
C
380 DO 400 I=1,43
      T(I)=SAVT(I)
400 CONTINUE
      DO 420 I=1,10
      TUG(I)=SAVTUG(I)
420 CONTINUE
      TUGAV=XTUGAV
      SQUG=XSQUG
      QEVAP=XQEVAP
      TOTL=XTOTL
      STORAT=XSTRAT
      QSHIV=XQSHIV
      QSTOR=XQSTOR
      GO TO 20
      END
      SUBROUTINE SHRT
      COMMON T(43),TUGAV,SQUG,QEVAP,TOTL,TDEWC,WORK,QSHIV,
      & STORAT,QSTOR,TCAB,VPDEW,U,TUG(10),ACE(10),ARE(10),
      & PCAB,RM,QLCG,C(41),TSET(43),TW,EUG,CLO,CpG,VEFF,G,
      & VCAR,DTIME,QBASAL
      COMMON/SHRTMN/EMAX(10),QRSEN1,QRSEN2,QRSEN3,QRSEN5,QRSEN6,
      * QSEN(10),QRAD(10)
      DIMENSION H(10)
      DATA H/.033,.026,2*.036,2*.033,2*.04,2*.036/
      TWR=TW+460.
      SQUGA=0.0
      SQUGW=0.0
      SQW=0.0
      TAVSKN=(0.446*T(8)+0.0826*T(12)+0.0826*T(16)+0.1945*T(20)+0.1945*
      & T(24))/0.9902

```

C.....

## C CALCULATION OF Q-RADIATED(GRAD) AND Q-SENSIBLE(QSEN)

```

C .....
DO 60 I=1,10
  J=4*I
  TUGR=TUG(I)+460.
  HC=H(I)*ACE(I)*SQRT(PCAB*VCAB)
  IF(G.LE.0.0)GO TO 10
  HC1=0.06*ACE(I)*(PCAB+.2*G*ABS(TUG(I)-TCAB))*.25
  IF(HC1.GT.HC)HC=HC1
10  HK=0.1713E-8*ARE(I)*EUG*(TUGR*.3+TUGR*.2*TWR+TUGR*TWR*.2+
  $TWR*.3)
  IF(I.LT.2.OR.I.GT.6)GO TO 20
  IF(CLO.LT.0.01)GO TO 20
  TUG(I)=(HR*TW+HC*TCAB+ACE(I)/CLO*T(J))/(HR+HC+ACE(I)/CLO)
  GO TO 40
20  TUG(I)=T(J)
40  QUGW=HR*(TUG(I)-TW)
  QUGA=HC*(TUG(I)-TCAB)
  SQUGW=SQUGW+QUGW
  SQUGA=SQUGA+QUGA
  QSEN(I)=QUGA
  GRAD(I)=QUGW
60  CONTINUE

```

C .....  
C

## C CALCULATION OF RESPIRATORY SENSIBLE

```

C .....
QRSEN1=0.5*0.0418*PCAB*144.0/(48.3*(TCAB+459.69))*RM*CPG*((0.385*T
, (1)+0.086*T(2)+0.0287*T(3)+0.238*T(5)+0.2615*T(6))-TCAB)
QRSEN2 = 0.172 * QRSEN1
QRSEN3 = 0.0574 * QRSEN1
QRSEN6 = 0.523 * QRSEN1
QRSEN5 = 0.476 * QRSEN1
QRSEN1=0.771*QRSEN1

```

C  
C

```

SQUG = SQUGA + SQUGW + SQW + QRSEN1 + QRSEN5 + QRSEN2 + QRSEN3 +
,QRSEN6

```

```

TUGAV=0.3317*TUG(2)+0.104*(TUG(3)+TUG(4))+0.23015*(TUG(5)+TUG(6))

```

C .....  
C

## C CALCULATE MAXIMUM EVAPORATION RATE

C .....  
C

```

DO 65 I=1,10
  J=4*I
  VPTUG=VPT(TUG(I))
  HE=0.126*ACE(I)*(TCAB+460.)*.04*VEFF/100.*SQRT(VCAB*PCAB)
  IF(G.LE.0.0)GO TO 65
  HE1=1.32*ACE(I)*(TCAB+460.)/PCAB*(PCAB*G*(ABS(.005*PCAB*TUG(I)-
  $TCAB)+1.02*(VPT(TUG(I))-VPDEW)))*.25
  IF(HE1.GT.HE)HE=HE1
65  IF(I.LT.2.OR.I.GT.6)GO TO 70
  IF(CLO.LT.0.01)GO TO 70
  HECL=22.36*ACE(I)*(T(J)+460.)*.0.81/(CLO*PCAB)

```

```
EMAX(1)=HE*HECL/(HE+HECL)*(VPT(T(J))-VPDEW)
```

```
GO TO 75
```

```
70 EMAX(1)=HE*(VPT(T(J))-VPDEW)
```

```
75 IF(EMAX(1).LT.0.0) EMAX(1)=0.0
```

```
80 CONTINUE
```

```
CALL MANT
```

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```
QSTOR=0.
```

```
DO 100 I=1,41
```

```
QSTOR=QSTOR+C(I)*(T(I)-TSET(I))
```

```
100 CONTINUE
```

```
STORAT=RM=(SQUGA+SQUGW+SQW+TOTL+QRSEN1+QRSEN2+QRSEN3+QRSEN4+
```

```
QRSEN5)+U+QSHIV
```

```
SCABC = QRSEN1 + QRSEN5 + QRSEN2 + QRSEN3 + QRSEN6 + SQUGA
```

```
SCAB1=SQUGA+SQUGW
```

```
RETURN
```

```
END
```

```
SUBROUTINE MANT
```

```
COMMON T(43),TUGAV,SQUG,QEVAP,TOTL,TDEWC,WORK,QSHIV,
```

```
& STORAT,QSTOR,TCAB,VPDEW,U,TUG(10),ACE(10),ARE(10),
```

```
& PCAR,RM,QLCG,C(41),TSET(43),TW,EUG,CLO,CPG,VEFF,G,
```

```
& VCAB,DTIME,QBASAL
```

```
COMMON/SHRTMN/EMAX(10),QRSEN1,QRSEN2,QRSEN3,QRSEN5,QRSEN6,
```

```
QSEN(10),QGRAD(10)
```

```
COMMON/DIAG/QCONV(40),QCOND(40),BF(40),QMET(40),TEST(41),WARM(41),
```

```
COLD(41),QDIF(10),QLAT(10)
```

```
DIMENSION SWTFAC(10),FACTOR(40)
```

```
DIMENSION BFB(40),QB(40),WORKM(10),CHILM(10),SKINV(10),SKINC(10),
```

```
SKINS(10)
```

```
DATA SWTFAC/0.6,0.05,0.05,0.08,0.08,0.01,0.01,0.01,0.01,0.01,0.01/
```

```
DATA CSW,SSW,PSW,CDIL,SDIL,PDIL,CCON,SCON,PCON,CCHIL,SCHIL,PCHIL
```

```
/705,0.63,9,0.0,143,9.2,0.0,2.78,2.78,0.0,0.0,0.0,0.25,7/
```

```
DATA BFB/105.6,0.594,0.264,3.7,510.0,14.08,5.06,4.62,0.759,1.364,
```

```
0.352,0.55,0.759,1.364,0.352,0.55,2.32,4.07,0.88,3.135,
```

```
2.32,4.07,0.88,3.135,0.11,0.055,0.055,2.2,0.11,0.055,
```

```
0.055,2.2,0.165,0.033,0.088,3.3,0.165,0.033,0.088,3.3/
```

```
DATA QB/.1604,.0039,.0018,.0009,.5622,.0914,.0335,.0044,.0049,
```

```
.0089,.0023,.0008,.0049,.0089,.0023,.0008,.0160,.0265,
```

```
.0057,.0019,.0160,.0265,.0057,.0019,.0006,.0002,.0004,
```

```
.0003,.0006,.0002,.0004,.0003,.0010,.0002,.0005,.0004,
```

```
.0010,.0002,.0005,.0004/
```

```
DATA WORKM/0.0,0.3,0.04,0.04,0.3,0.3,0.005,0.005,0.005,0.005/
```

```
DATA CHILM/0.023,0.948,0.00165,0.00165,0.0095,0.0095,0.00115,
```

```
0.00115,0.00115,0.00115/
```

```
DATA SKINV/0.132,0.322,0.0475,0.0475,0.115,0.115,0.061,0.061,
```

```
0.05,0.05/
```

```
DATA SKINC/0.05,0.15,0.025,0.025,0.025,0.025,0.175,0.175,0.175,
```

```
0.175/
```

```
DATA SKINS/0.081,0.482,2*0.077,2*0.1095,2*0.0155,2*0.0175/
```

```
DATA FACTOR/8.85,12.82,22.60,0.0,3.09,10.70,28.05,0.0,3.18,8.32,
```

```
22.80,0.0,3.18,8.32,22.80,0.0,5.75,18.70,33.50,0.0,
```

```
5.75,18.70,33.50,0.0,4.50,8.32,9.41,0.0,4.50,8.32,
```

```
9.41,0.0,5.54,13.36,11.93,0.0,5.54,13.36,11.93,0.0/
```



C SWEAT, SHIVER, CONSTRICTION, DILATION CALCULATIONS

C .....

DO 80 I=1,40  
 TEST(I)=T(I)-TSET(I)  
 WARM(I)=0.0  
 COLD(I)=0.0  
 IF (TEST(I)) 20,40,60  
 20 COLD(I)=-TEST(I)  
 40 GO TO 80  
 60 WARM(I)=TEST(I)  
 80 CONTINUE

ORIGINAL PAGE IS  
 OF POOR QUALITY

C TAVSK=T(42)  
 WARMS=0.0827\*WARM(4)+0.587\*WARM(8)+0.0411\*WARM(12)+0.0411\*WARM(16)  
 +0.093\*WARM(20)+0.093\*WARM(24)+0.011075\*WARM(28)+0.011075\*  
 WARM(32)+0.01995\*WARM(36)+0.01995\*WARM(40)  
 COLDS=0.0827\*COLD(4)+0.587\*COLD(8)+0.0411\*COLD(12)+0.0411\*COLD(16)  
 +0.093\*COLD(20)+0.093\*COLD(24)+0.011075\*COLD(28)+0.011075\*  
 COLD(32)+0.01995\*COLD(36)+0.01995\*COLD(40)  
 WARMH=0.417\*WARM(6)+0.095\*WARM(10)+0.095\*WARM(14)+0.1965\*WARM(18)+  
 0.1965\*WARM(22)  
 COLDM=0.417\*COLD(6)+0.095\*COLD(10)+0.095\*COLD(14)+0.1965\*COLD(18)+  
 0.1965\*COLD(22)  
 SWEAT=CSW\*WARM(I)+SSW\*WARMS+PSW\*WARM(I)\*WARMS  
 DILAT=CDIL\*WARM(I)+SDIL\*WARMS+PDIL\*WARM(I)\*WARMS  
 STRIC=CCON\*COLD(I)+SCON\*COLDS+PCON\*COLD(I)\*COLDS  
 CALL CQSH(T(I),QSHIV,TAVSK,QBASAL)

C .....

C CALCULATION OF RESPIRATORY LATENT

C .....

QLAT1=.5\*0.0418\*PCAB\*144./(48.3\*(TCAB+459.69))\*RM\*(VPT(0.385\*  
 \*T(1)+0.086\*T(2)+0.0287\*T(3)+0.238\*T(5)+0.2615\*T(6))-0.8\*VPDEW)  
 \*((18.0\*1040.0)/(32.0\*PCAB))  
 QLAT2=0.172\*QLAT1  
 QLAT3=0.0574\*QLAT1  
 QLAT5=0.476\*QLAT1  
 QLAT6=0.523\*QLAT1  
 QLAT1=0.771\*QLAT1  
 QR=QLAT1+QLAT2+QLAT3+QLAT5+QLAT6

C .....

C SKIN DIFFUSION

C .....

DO 100 I=1,10  
 QDIF(I)=6.66\*(VPT(TUG(I))-VPDEW)\*ACE(I)  
 100 CONTINUE  
 120 CONTINUE

C .....

C QLATENT(QLAT) CALCULATIONS

C .....



```

DO 160 I=1,10
J=4+I
QLAT(I)=QDIF(I)*SKINS(I)*SWEAT*2.0*((T(J)-TSET(J))/4.)
IF (QLAT(I).GT.EMAX(I)) GO TO 140
GO TO 160
140 QLAT(I)=EMAX(I)
160 CONTINUE
QD=0.0
TOTL=QR
DO 180 I=1,10
QD=QD+QDIF(I)
180 TOTL=TOTL+QLAT(I)
QEVAP=TOTL-QR-QD
C.....
C BLOOD FLOW CALCULATIONS
C.....
DO 200 I=1,10
N=4+I-3
BF(N)=BFB(N)
QMET(N)=QB(N)*QBASAL
QMET(N+1)=QB(N+1)*QBASAL+WORKM(I)*WORK+CHILM(I)*QSHIV
BF(N+1)=BFB(N+1)+QMET(N+1)-QB(N+1)*QBASAL
QMET(N+2)=QB(N+2)*QBASAL
BF(N+2)=BFB(N+2)
QMET(N+3)=QB(N+3)*QBASAL
BF(N+3)=(BFB(N+3)+SKINV(I)*DILAT)/(1.0+SKINC(I)*STRIC)
200 CONTINUE
TSBF=BF(4)+BF(8)+BF(12)+BF(16)+BF(20)+BF(24)+BF(28)+BF(32)+BF(36)
      +BF(40)
C-----
C CHECK FOR NEGATIVE BLOOD FLOW
C-----
DO 220 I=1,40
220 IF (BF(I).LT.0.0) BF(I)=0.0
C-----
C QCONV(I)=CONVECTION FROM BLOOD TO EACH NODE
C QCOND(I)=CONDUCTION BETWEEN ADJACENT NODES
C-----
DO 240 I=1,40
QCONV(I)=BF(I)*(T(41)-T(I))
QCOND(I)=FACTOR(I)*(T(I)-T(I+1))
240 CONTINUE
C.....
C TEMPERATURE CALCULATIONS
C.....
C-----
C CALCULATE TEMP OF HEAD CORE,T(1), AND TRUNK CORE,T(5).
C-----
T(1)=T(1)+DIME/C(1)*(QMET(1)-QLAT1+QCONV(1)-QCOND(1)-QRSEN1)
T(5)=T(5)+DIME/C(5)*(QMET(5)-QLAT5+QCONV(5)-QCOND(5)-QRSEN5)
C-----
C CALCULATE TEMPERATURES OF REMAINING CORES --ARM(9+13),LEG(17+21),
C HAND(25+29),AND FOOT(33+37)
C-----
DO 260 I=9,37,4
T(I)=T(I)+DIME/C(I)*(QMET(I)+QCONV(I)-QCOND(I))
260 CONTINUE

```

```

C-----
C  CALCULATE THE TEMPERATURES OF THE MUSCLE --HEAD(2),TRUNK(6),ARM(10+
C      14),LEG(18+22),HAND(26+30),FOOT(34+38)
C-----
      T(2)=T(2)+DTIME/C(2)*(QCOND(1)+QMET(2)-QLAT2+QCONV(2)-QCOND(2)-
      •   QRSEN2)
      T(6)=T(6)+DTIME/C(6)*(QCOND(5)+QMET(6)-QLAT6+QCONV(6)-QCOND(6)-
      •   QRSEN6)
      DO 280 I=10,38,4
      T(I)=T(I)+DTIME/C(I)*(QCOND(I-1)+QMET(I)+QCONV(I)-QCOND(I))
280  CONTINUE
C-----
C  CALCULATE TEMPERATURES OF THE FAT LAYER --HEAD(3),TRUNK(7),ARM(11+15)
C      LEG(19+23),HAND(27+31),FOOT(35+39)
C-----
      T(3)=T(3)+DTIME/C(3)*(QCOND(2)+QMET(3)-QLAT3+QCONV(3)-QCOND(3)-
      •   QRSEN3)
      DO 300 I=7,39,4
      T(I)=T(I)+DTIME/C(I)*(QCOND(I-1)+QMET(I)+QCONV(I)-QCOND(I))
300  CONTINUE
C-----
C  CALCULATE TEMPERATURES OF THE SKIN --HEAD(4),TRUNK(8),ARM(12+16),
C      LEG(20+24),HAND(28+32),FOOT(36+40)
C-----
      DO 320 I=4,40,4
      J=I/4
      T(I)=T(I)+DTIME/C(I)*(QCOND(I-1)+QMET(I)-QLAT(J)+QCONV(I)
      •   -QSEN(J)-QRAD(J)-QLCG)
320  CONTINUE
C-----
C  CALCULATE TEMP OF CENTRAL BLOOD --(41)
C-----
      SQCONV = 0.0
      DO 340 I=1,40
      SQCONV=SQCONV+QCONV(I)
340  CONTINUE
      T(41)=T(41)+DTIME/C(41)*SQCONV
C-----
C  CALCULATE AVERAGE SKIN TEMPERATURE(42) BASED ON PERCENTAGE OF
C  TOTAL SKIN AREA FOR EACH SKIN NODE * THAT NODES TEMPERATURE
C-----
      T(42)=0.07*T(4)+0.3602*T(8)+0.06705*T(12)+0.06705*T(16)+0.1587*
      •   T(20)+0.1587*T(24)+0.025*T(28)+0.025*T(32)+0.0343*T(36)+
      •   0.0343*T(40)
      T(43)=0.02325*T(2)+0.549*T(6)+0.0527*T(10)+0.0527*T(14)+0.1592*
      •   T(18)+0.1592*T(22)+0.00115*T(26)+0.00115*T(30)+0.00115*
      •   T(34)+0.00115*T(38)
      TBF=0.0
      DO 360 I=1,40
360  TBF=TBF+BF(I)
      PULSE=5.926*TBF/60.0
      RETURN
      END
      SUBROUTINE CQSH(TIC,QSHIV,TAVSK,QBASAL)
      COMMON/NSHIV/TAVG,TC,RMX
      CALL TCF(TC,TIC,0)
      CALL TCF(TAVG,TAVSK,0)

```

TC=TC-(.1-(((37.0-TC)\*.1.7)\*\*2.)/10.)

RMX=22221.-414.2\*(TC)\*TAVG\*(-1933.2+53.66\*(TC))

6+TAVG\*\*2\*(46.45-1.289\*(TC))

C CONVERTS METABOLIC RATE FROM CAL/SEC TO BTU/MR

RMX=RMX\*3.6\*3.97

QSHIV=RMX-QBASAL

IF (QSHIV.LE.0.0)QSHIV=0.0

RETURN

END

SUBROUTINE TCF (TC,TF,IFL)

IF (IFL.NE.0)GO TO 65

TC=(TF-32.)\*5./9.

RETURN

65 TF=TC\*9./5.+32

RETURN

END

FUNCTION VPT(T)

C FUNCTION TO CALCULATE VAPOR PRESSURE AT TEMP=T

X=647.27-(T+460.)/1.8

TEMP=X+1.8/(T+460.)\*(1.3,244+5.868E-3\*X+1.170E-8\*X\*\*3)

6/(1.+2.188E-3\*X)

VPT=3207./10.\*\*TEMP

RETURN

END

SUBROUTINE GVAR(NI,NA,NN)

DIMENSION NI(8),NA(8),KA(55)

DATA (KA(1),I=1,5)/' T(1) T(2) T(3) T(4) T(5)'/

DATA (KA(1),I=6,10)/' T(6) T(7) T(8) T(9) T(10)'/

DATA (KA(1),I=11,15)/' T(11) T(12) T(13) T(14) T(15)'/

DATA (KA(1),I=16,20)/' T(16) T(17) T(18) T(19) T(20)'/

DATA (KA(1),I=21,25)/' T(21) T(22) T(23) T(24) T(25)'/

DATA (KA(1),I=26,30)/' T(26) T(27) T(28) T(29) T(30)'/

DATA (KA(1),I=31,35)/' T(31) T(32) T(33) T(34) T(35)'/

DATA (KA(1),I=36,40)/' T(36) T(37) T(38) T(39) T(40)'/

DATA (KA(1),I=41,45)/' T(41) T(42) T(43) TUGAV SQUG'/

DATA (KA(1),I=46,50)/' QEVAP TOTL TDEWC WORK QSHIV'/

DATA (KA(1),I=51,55)/'STORAT QSTOR TCAB VPDEW U'/

WRITE(6,10)

10 FORMAT(/'PLEASE ENTER ITEMS TO BE PLOTTED BY INDEX NO. (12)')

DO 30 I=1,8

GO TO 15

13 WRITE(6,14)

14 FORMAT(' \*\*\*\*\* READ ERROR')

15 READ (5,20,ERR=13) NI(I)

20 FORMAT(I2)

IF (NI(I).LT.1) GO TO 40

IF (NI(I).GT.55) GO TO 13

M=NI(I)

NA(I)=KA(M)

WRITE(6,25) NI(I),NA(I)

25 FORMAT(' \*\*\*\*\*',I3,2X,A6)

30 CONTINUE

40 NN=I-1

RETURN

END

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OF POOR QUALITY

ORIGINAL PAGE 15  
DE POOR QUALITY

APPENDIX 2

EXAMPLE RUN

QXOT RUN

DO YOU WANT GRAPHIC INSTEAD OF TABULAR OUTPUT? (Y/N)  
>Y

PLEASE ENTER ITEMS TO BE PLOTTED BY INDEX NO. (12)

>01  
##### 1 T(1)  
>42  
##### 42 T(42)  
>50  
##### 50 QSHIU  
>51  
##### 51 STORAT  
>52  
##### 52 QSTOR  
,

INPUT DATA USING NAMELIST \$INPUT

>@ADD TRDAT  
> SEND

SIMPUT

```

RH      = .27000000E+03
OBS     = .27000000E+03
UEFF    = .50000000E+01
AC       = .19500000E+02
AR       = .15500000E+02
TCAB    = .80000000E+02
TW       = .80000000E+02
TDENC   = .67000000E+02
UCAB    = .50000000E+02
UEFF    = .15000000E+02
PCAB    = .14700000E+02
G        = .10000000E+01
CLOU    = .10000000E+01
EUC      = .90000000E+00
CPG      = .22000000E+00
DT       = .50000000E-01
PRINTI  = .20000000E+01
SETI     = .24000000E+03
MCASES  =      +0

```

SEND

# INITIAL CONDITIONS

TMINS	HEADCORE	AUGSKIN	TUGAV	BLOOD	QEVAP	INSENS
STORAT	QSHIU	QSTOR	TCAB			
.0	90.00	95.00	95.00	90.50	.00	.00
.00	.00	00.00	67.00			
240.0	90.24	93.27	05.03	90.11	-.00	63.67
-0.00	-69.00	00.00	67.00			

INPUT DATA USING NAMELIST SIMPUT

```

MCASES=1
> TCAB=40.
> TH=40.
> SEND
SIMPUR
RM      = .27000000E+03
OBS      = .27000000E+03
UEFF     = .50000000E+01
AC       = .19500000E+02
AR       = .15500000E+02
TCAB     = .40000000E+02
TH       = .40000000E+02
TDENC    = .67000000E+02
UCAB     = .50000000E+02
UEFF     = .15000000E+02
PCAB     = .14700000E+02
G        = .10000000E+01
CLOU     = .10000000E+01
EUG      = .90000000E+00
CPG      = .22000000E+00
DT       = .50000000E-01
PRINTI   = .20000000E+01
SETI     = .24000000E+03
MCASES   = +1

```

```
SEND
```

# IMPOSED CONDITIONS

```

TNINS      HEADCORE AUGSKIN TUGAU      GEUAP      INSENS
ISTORAT    OSHIU  OSTOR  TCAB      TDENC
TYPE SHIFT-OUT (SO) AND RETURN-->

```

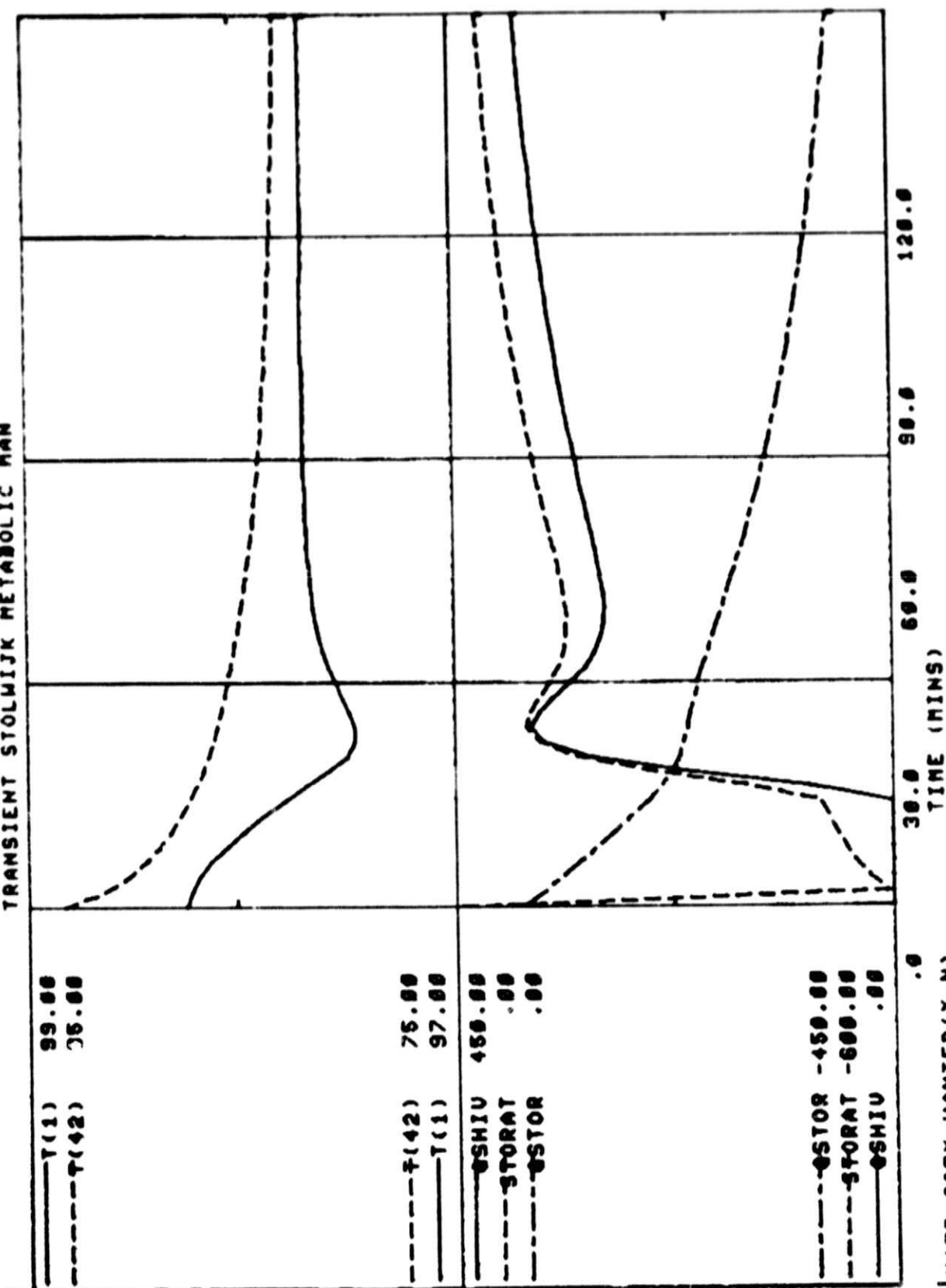
```

      GRAPHIC OUTPUT(Y,N,S),TIME INTERVALS,STARTX,STOPX,(A2,JF6.0)..
>Y 4. 0. 120.
  T(1)      Y SCALE      (A4,8X,F4.0,2F6.0)
  PLOT(Y,N,S) LOC HIGH LOW ...
>Y 1. 99. 97.
  T(42)     Y SCALE      (A4,8X,F4.0,2F6.0)
  PLOT(Y,N,S) LOC HIGH LOW ...
>Y 1. 95. 75.
  QSHIU     Y SCALE      (A4,8X,F4.0,2F6.0)
  PLOT(Y,N,S) LOC HIGH LOW ...
>Y 2. 450. 0.
  STORAT    Y SCALE      (A4,8X,F4.0,2F6.0)
  PLOT(Y,N,S) LOC HIGH LOW ...
>Y 2. 0. -600.
  QSTOR     Y SCALE      (A4,8X,F4.0,2F6.0)
  PLOT(Y,N,S) LOC HIGH LOW ...
>Y 2. 0. -450.

```



## TRANSIENT STOLWIJK METABOLIC MAN



HARD COPY WANTED(Y,N)...